$\begin{array}{c} \mathrm{ECE}\ 4213/5213 \\ \mathrm{Test}\ 2 \end{array}$

Thursday, December 3, 2009 12:00 PM - 1:15 PM

Fall 2009			Name: SOLUTION
Dr. Havli	icek		Student Num:
notes, an	d a clean	copy of the formula she	may also use a calculator, a clean copy of the course eet from the course web site. Other materials are plete the test. All work must be your own.
Student counts 25		l for undergraduate	credit: work any four problems. Each problem
	s enrolled	l for graduate credit	: work all five problems. Each problem counts 20
points.			
SH	OW ALL	OF YOUR WORK for	maximum partial credit! GOOD LUCK!
SCO	RE:		
1.	(25/20) _		
2.	(25/20) _		
3.	(25/20) _		
4	(25/20)		
4.			
	(25/20) _		
	(25/20) _		
5.	(25/20) _ 		

1. 25/20 pts. An LTI digital filter H has transfer function

$$H(z) = \frac{(1 - 5z^{-1})(1 - 3z^{-1})}{(1 - \frac{1}{2}z^{-1})(1 - \frac{1}{4}z^{-1})}, \ |z| > \frac{1}{2}.$$

Give Direct Form I and Direct Form II realizations of H(z).

$$H(z) = \frac{1 - 8z^{-1} + 15z^{-2}}{1 - \frac{3}{4}z^{-1} + 16z^{-2}}$$

$$TEXT (8.23): Po = 1 \quad P_1 = -8 \quad P_2 = 15$$

$$d_1 = -34 \quad d_2 = \frac{1}{8}$$

DIRECT FORM I

[Fig 8.13(a)]

7(CM)

21

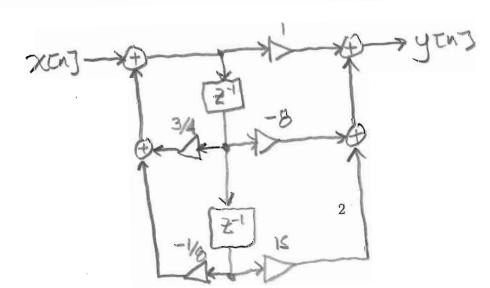
34

21

15

15

DIRECT FORM I [Fig 8. 14(a)]



2. 25/20 pts. An IIR digital filter H has input x[n] and output y[n] related by the difference equation

$$y[n] - \frac{3}{4}y[n-1] + \frac{1}{8}y[n-2] = x[n] - 8x[n-1] + 15x[n-2].$$

Y(2) 1-3-1+ 32.2

The system H is LTI, causal, and BIBO stable. But it is **not** minimum phase.

Find a new LTI digital system G such that:

- (a) G(z) has minimum phase.
- (b) G is both causal and BIBO stable.

(c)
$$|G(e^{j\omega})| = |H(e^{j\omega})| \ \forall \ \omega \in \mathbb{R}.$$

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.

$$|f(z)| = \frac{f(z)}{\chi(z)} = \frac{|-8z^{-1} + 15z^{-2}|}{|-\frac{3}{4}z^{-1} + \frac{1}{8}z^{-2}|} = \frac{(1-3z^{-1})(1-5z^{-1})}{(1-\frac{1}{2}z^{-1})(1-4z^{-1})}, |z| > \frac{1}{2}$$
The two zeros at $z=3$ and $z=5$ are both such that

The two zeros at z=3 and z=5 are both outside the unit circle. Reflect them inside by factoring aut a pair of allpass sections.

$$= \frac{(3-z^{-1})(5-z^{-1})}{(1-\frac{1}{2}z^{-1})(1-\frac{1}{4}z^{-1})} \frac{1-3z^{-1}}{3-z^{-1}} \frac{1-5z^{-1}}{5-z^{-1}}$$

=
$$\frac{15(1-\frac{1}{3}z^{-1})(1-\frac{1}{5}z^{-1})}{(1-\frac{1}{2}z^{-1})(1-\frac{1}{4}z^{-1})}$$
 $\frac{1-3z^{-1}}{3-z^{-1}}$ $\frac{1-5z^{-1}}{5-z^{-1}}$ $\frac{1-5z^{-1}}{5-z^{-1}}$ all pass all pass

$$G(z) = \frac{15(1-\frac{1}{3}z^{-1})(1-\frac{1}{5}z^{-1})}{(1-\frac{1}{2}z^{-1})(1-\frac{1}{4}z^{-1})}$$

3. 25/20 pts. An FIR digital filter H has impulse response

$$h[n] = \delta[n] - \delta[n-1] + \frac{1}{2}\delta[n-2] - \frac{1}{2}\delta[n-3] + \frac{1}{4}\delta[n-4] - \frac{1}{4}\delta[n-5].$$

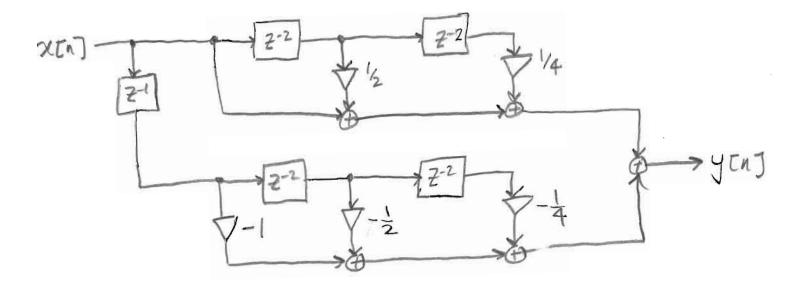
Show the block diagram for a polyphase realization of H(z) using L=2 branches (e.g., two polyphases).

$$H(z) = 1 - z^{-1} + \frac{1}{2}z^{-2} - \frac{1}{2}z^{-3} + \frac{1}{4}z^{-4} - \frac{1}{4}z^{-5}$$

$$= \left(1 + \frac{1}{2}z^{-2} + \frac{1}{4}z^{-4}\right) - z^{-1}\left(1 + \frac{1}{2}z^{-2} + \frac{1}{4}z^{-4}\right)$$

$$= \left(E_{0}(z^{2})\right) - E_{1}(z^{2}) \qquad Fram \qquad (8.18).$$

Realize as in Fig. 8.7(c) with the basic FIR structure of Fig. 8.5(a):



passband edge freq.	$\Omega_p = \pi \text{ rad/sec}$
stopband edge freq.	$\Omega_s = 2\pi \text{ rad/sec}$
max. stopband ripple	$1/A = 1/\pi$
passband equiripple	$1/\sqrt{1+\varepsilon^2} = 0.9$

E2 = 100-81 = 19

E = 0,4843Z [00] &

Give the analog filter transfer function $H_a(s)$.

Hint: The design formulas for the analog Type I Chebyshev filter are given on pages

(4.43):
$$N = \frac{191 \text{ and } 192 \text{ of the text.}}{\left(\frac{4.43}{3}\right)!} = \frac{191 \text{ and } 192 \text{ of the text.}}{\left(\frac{2.50279}{3.31696}\right)!} = \frac{10.90043}{10.31696} = \frac{10.90043}{10.$$

$$(4.456)$$
: $\gamma = [1 + \sqrt{1 + \epsilon^2}]^{\frac{1}{2}} = 2.08780 \boxed{03}$ $5 = \frac{\gamma^2 + 1}{2\gamma} = 1.28339 \boxed{64}$

$$\xi = \frac{Y^2 - 1}{ZY} = 0.804412$$
 F5

$$(4.45a): \sigma_{1} = -\pi \xi \sin \frac{\pi}{4} = -1.78695 \quad \text{EG}$$

$$\Omega_{1} = \pi \xi \cos \frac{\pi}{4} = 2.85097 \quad \text{EG}$$

$$\sigma_{2} = -\pi \xi \sin \frac{3\pi}{4} = -1.78695 \quad \text{EG}$$

$$\Omega_{2} = \pi \xi \cos \frac{3\pi}{4} = -2.85097 \quad \text{EG}$$

$$\Omega_{2} = \pi \xi \cos \frac{3\pi}{4} = -2.85097 \quad \text{EG}$$

(4.44):
$$P_1 = \sigma_1 + j\Omega_1 = -1.78695 + j2.85097$$

 $P_2 = \sigma_2 + j\Omega_2 = -1.78695 - j2.85097$

The sentence above (4.44) Tells you that Hals) is given by (4.36):

$$H_q(s) = \frac{C}{(s-P_1)(s-P_2)} = \frac{C}{s^2 - (P_1 + P_2)s + P_1 P_2}$$

$$= \frac{C}{S^2 - Z\sigma_1 S + \sigma_1^2 + \Omega_1^2 5} \quad (\#) \qquad \longrightarrow$$

More Workspace for Problem 4...

To solve C, note that the peak of HaLR) occurs at N=0 where Halo = 1:

$$1 = H_{a(0)} = \frac{C}{\sigma_{1}^{2} + \Omega_{1}^{2}} \Rightarrow C = \sigma_{1}^{2} + \Omega_{1}^{2} = 11.3212$$
 [5]

Fram (*) on p.5,

$$H_a(s) = \frac{\sigma_1^2 + \Omega_1^2}{s^2 - 2\sigma_1 s + \sigma_1^2 + \Omega_1^2} = \frac{11.3212}{s^2 + 3.57391s + 11.3212}$$

$$H_a(s) = \frac{11.3212}{s^2 + 3.57391s + 11.3212}$$

$$= [s-(-1.78695+j2.85097)][s-(-1.78695-j2.85097)]$$

5. 25/20 pts. Use the bilinear transform with T=2 and Steps 1-5 of the first approach given at the top of page 501 of the text to design a highpass digital Butterworth filter meeting the following specification:

passband edge freq.	$\hat{\omega}_p = 0.75\pi \text{ rad/sample}$
stopband edge freq.	$\hat{\omega}_s = 0.25\pi \text{ rad/sample}$
max. passband ripple	$\varepsilon = 0.75$
max. stopband ripple	A=4

Let $H_D(e^{j\hat{\omega}})$ and $H_D(z)$ be the frequency response and transfer function of the desired digital highpass filter.

Let $\hat{\omega}_p$ and $\hat{\omega}_s$ be the critical frequencies of the desired digital highpass filter given in the table above.

Let $\hat{\Omega}_p$ and $\hat{\Omega}_s$ be the critical frequencies of the equivalent analog highpass filter. Call the transfer function of this filter $H_D(\hat{s})$.

Let Ω_p and Ω_s be the critical frequencies of the prototype analog lowpass filter. Call the transfer function of this filter $H_a(s)$.

(a) 3/3 pts. Step 1: use (9.18) with T=2 to prewarp the digital critical frequencies $\hat{\omega}_p$ and $\hat{\omega}_s$ and obtain the analog critical frequencies $\hat{\Omega}_p$ and $\hat{\Omega}_s$ of the equivalent analog highpass filter.

$$\hat{\Lambda}_{p} = \tan(\frac{\omega_{p}}{2}) = \tan(\frac{3\pi}{8}) = 2.41421 \text{ rad/sec}$$

$$\hat{\Lambda}_{s} = \tan(\frac{\omega_{s}}{2}) = \tan(\frac{\pi}{8}) = 0.414214 \text{ rad/sec}$$

(b) 4/3 pts. Step 2: obtain the critical frequencies of the prototype analog lowpass filter by letting $\Omega_p = 1$ and using the transformation (4.63) to solve for Ω_s . Hint: (4.63) gives you the stopband edge frequency that is located on the negative frequency axis. Since the magnitude is even, you can multiply this by -1 to get the positive stopband edge frequency.

$$\Omega_{s} = \frac{1}{\hat{\Omega}_{s}} = \frac{1}{\hat{\Omega}_{s}} = -\frac{\hat{\Omega}_{p}}{\hat{\Omega}_{s}} = -\frac{2.41421}{0.414214} = -5.82843 \text{ rad/sec}$$

Problem 5 cont....

(c) 10/7 pts. Step 3: design the prototype analog lowpass Butterworth filter $H_a(s)$ using the design formulas on pages 189 and 190 of the text. As suggested on page 190, use (4.34b) to solve for Ω_C after you obtain the order using (4.35).

$$(4.35) N = \begin{cases} \frac{1}{2} \frac{\log \left[(\Lambda^{2} - 1)/\epsilon^{2} \right]}{\log \left(\Omega_{5}/\Omega_{p} \right)} = \begin{cases} \frac{1}{2} \frac{\log \left[15.16/5 \right]}{\log \left[5.82843 \right]} \\ = \begin{cases} \frac{1}{2} \frac{1.47597}{6.765552} = \left[0.931334 \right] = \frac{1}{4} \end{cases}$$

$$(4.34b) \frac{1}{A^{2}} = \frac{1}{16} = \frac{1}{1 + \frac{\Omega_{5}^{2}}{\Omega_{c}^{2}}} \Rightarrow 16 = \frac{1 + \frac{\Omega_{5}^{2}}{\Omega_{c}^{2}}}{15 = \frac{\Omega_{5}^{2}}{\Omega_{c}^{2}}}$$

$$\Omega_{c} = \frac{\Omega_{5}}{\sqrt{15}} = \frac{5.82843}{\sqrt{15}} = 1.50489$$

$$(4.37) R = R_{c} e^{\frac{1}{2} \left[\pi \left(1+2-1 \right)/2 \right]} = \Omega_{c} e^{\frac{1}{2} \pi} = -\Omega_{c} = -1.50489$$

$$(4.36) H_{a}(5) = \frac{R_{c}}{S - P_{1}} = \frac{\Omega_{c}}{S + \Omega_{c}} = \frac{1.50489}{S + 1.50489}$$

Problem 5 cont....

(d) 4/3 pts. Step 4: use (4.62) to convert the prototype lowpass filter $H_a(s)$ into the desired analog highpass filter $H_D(\hat{s})$.

$$H_D(\hat{s}) = H_a(\hat{s})\Big|_{\hat{s} = \frac{\Omega_P \Omega_P}{\hat{s}} = \frac{\Omega_P}{\hat{s}} = \frac{\Omega_C}{\hat{s}_P/\hat{s}} + \Omega_C$$

$$= \frac{\Omega_C \hat{s}}{\hat{\Omega}_P + \Omega_C \hat{s}} \frac{V_{\Omega_C}}{V_{\Omega_C}} = \frac{\hat{s}}{\hat{s} + \frac{\Omega_P}{\Omega_C}}$$

$$H_D(\hat{s}) = \frac{\hat{s}}{\hat{s} + 1.60424}$$

(e) 4/4 pts. Step 5: use the bilinear transform (9.14) with T=2 to obtain the transfer function $H_D(z)$ of the desired highpass digital filter.

$$H_{D}(z) = H_{D}(\hat{s}) \Big|_{\hat{s} = \frac{1-z^{-1}}{1+z^{-1}}} = \frac{\frac{1-z^{-1}}{1+z^{-1}}}{\frac{1-z^{-1}}{1+z^{-1}} + 1.60424} \frac{\frac{1+z^{-1}}{1+z^{-1}}}{\frac{1-z^{-1}}{1+z^{-1}} + 1.60424} \frac{\frac{1+z^{-1}}{1+z^{-1}}}{2.60424 + 0.60424z^{-1}}$$

$$= \frac{0.383989(1-z^{-1})}{1+0.232022z^{-1}}$$

